

# Diodes.

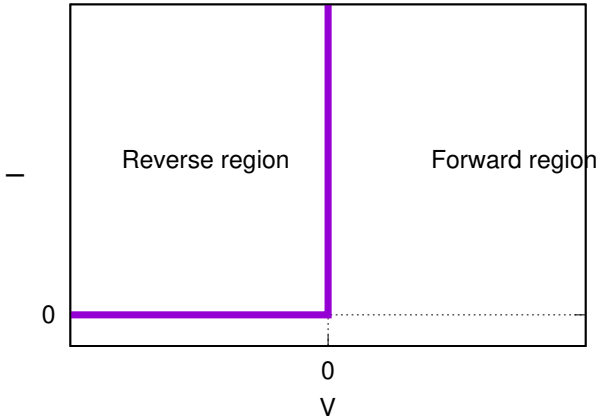
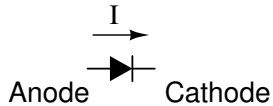
Eugeniy E. Mikhailov



WILLIAM & MARY

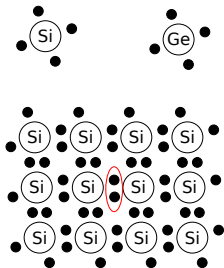
CHARTERED 1693

# Ideal diode



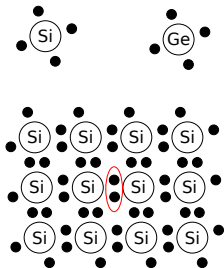
# Semiconductors and doping

## Pure semiconductor

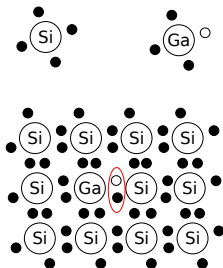


# Semiconductors and doping

Pure semiconductor

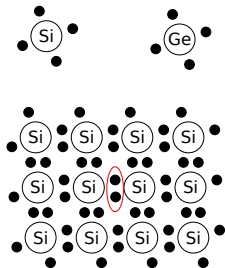


P-doped

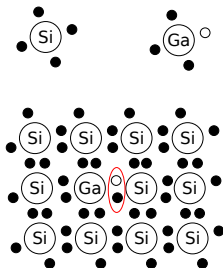


# Semiconductors and doping

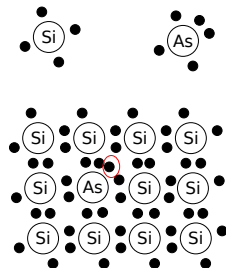
Pure semiconductor



P-doped

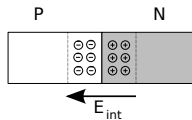


N-doped



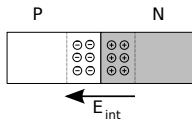
# PN-junction

No bias

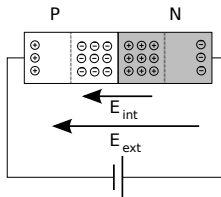


# PN-junction

No bias

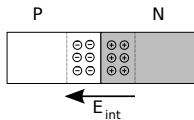


Reverse bias

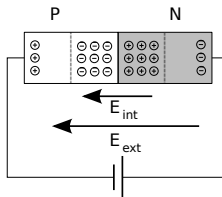


# PN-junction

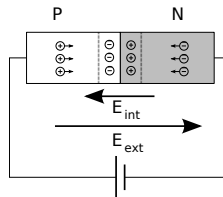
No bias



Reverse bias

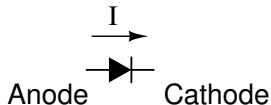


Forward bias





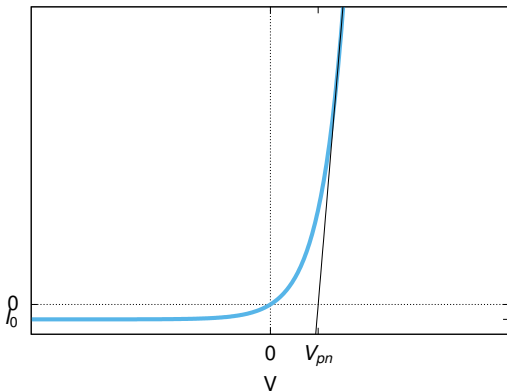
# Real diode



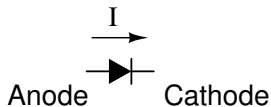
$$I(V) = I_0 \left( e^{V/(nV_T)} - 1 \right)$$

## Typical parameters

- saturation current  
 $I_0 = 1 \text{ nA}$
- thermal voltage  
 $V_T = \frac{kT}{q} =$   
25.85 mV at 300 K
- emission coefficient  
 $n = 1..2$



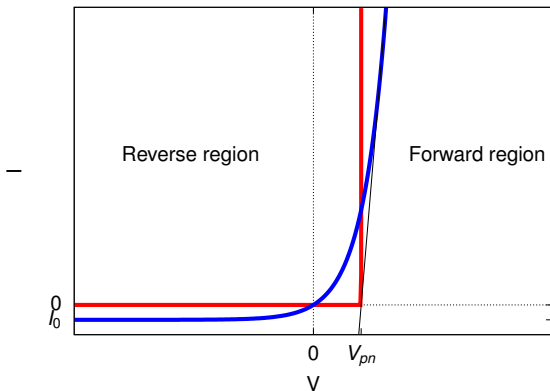
# Real diode



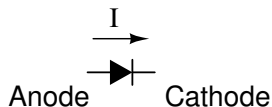
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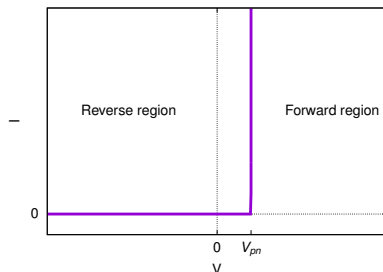


# Simplified diode

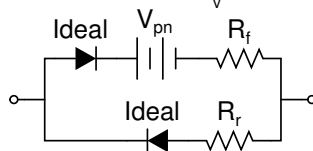


$V_{pn}$  diode P-N junction opening voltage

- $V_{pn} = 0.6$  V for Si
- $V_{pn} = 0.3$  V for Ge



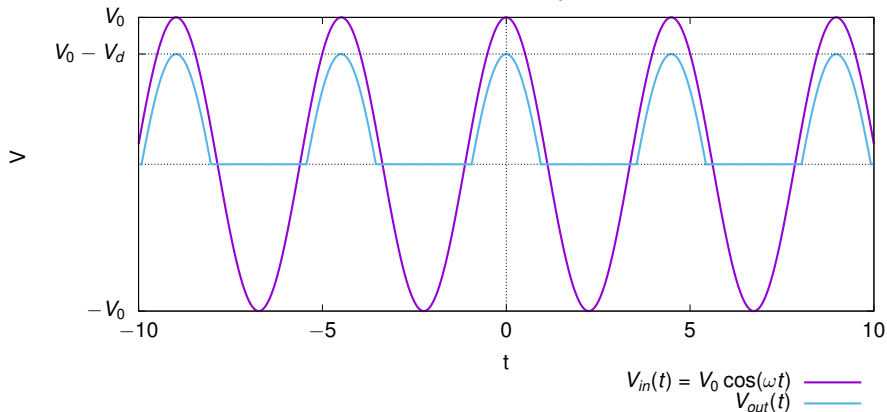
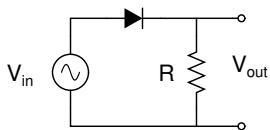
A bit more realistic diode  
( $R_r \gg R_f$ )



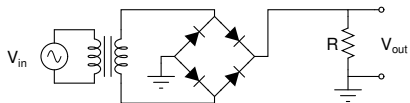
# Diodes applications

- Circuit Protection
- Rectification
  - current gate
  - half wave rectifier
  - full wave rectifier
  - Power Supplies
- Frequency manipulation
  - Frequency multiplier
  - Mixers
- and more ...
  - Voltage clamps
  - light emitting diodes (LED)
  - photo-diode

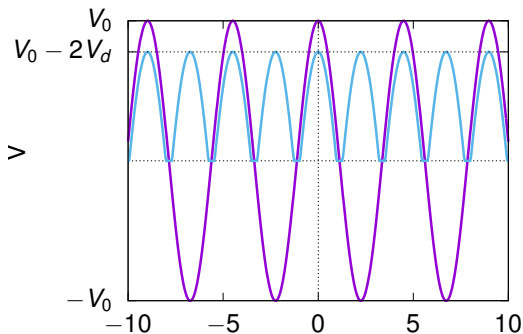
# Half-wave rectifier, current gate



# Full-wave rectifier: $V_{in} \gg V_d \rightarrow V_{out} \approx |V_{in}|$

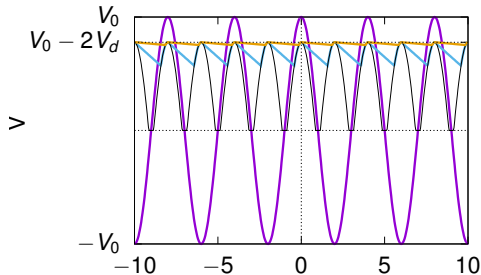
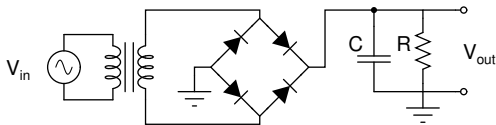


Why  
 $\max(V_{out}) = V_0 - 2V_d$  ?



$$V_{in}(t) = V_0 \cos(\omega t) \quad \text{— purple —}$$
$$V_{out}(t) \quad \text{— blue —}$$

# Full-wave rectifier filtered - power supply



$$\begin{aligned}
 V_{in}(t) &= V_0 \cos(\omega t) && \text{— (purple)} \\
 V_{out}(t), C1 &&& \text{— (light blue)} \\
 V_{rec}(t) &&& \text{— (grey)} \\
 V_{out}(t), C2 > C1 &&& \text{— (yellow)}
 \end{aligned}$$

Ripples size

$$V(t) = \frac{Q(t)}{C} = \frac{Q_{max} - \int_0^t I dt}{C}$$

$$= V_{max} - \int_0^t \frac{I}{C} dt$$

$$\Delta V = V_{max} - V(t) = \int_0^t \frac{I}{C} dt$$

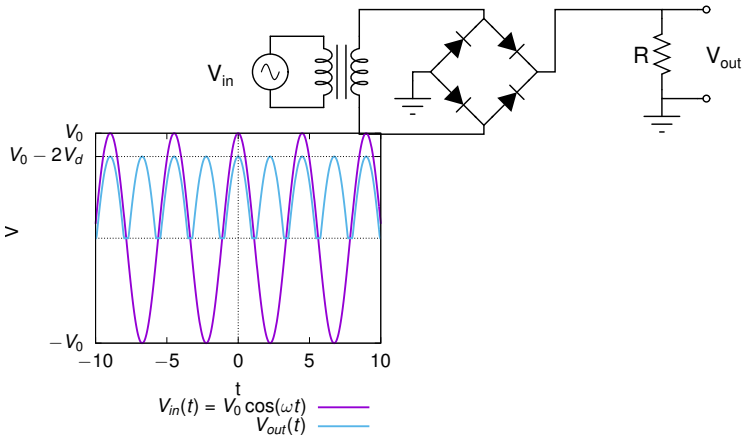
$$I \leq I_{max} = \frac{V_{max}}{R}$$

$$t \leq T = \frac{1}{2f_{in}}$$

$T \ll RC$

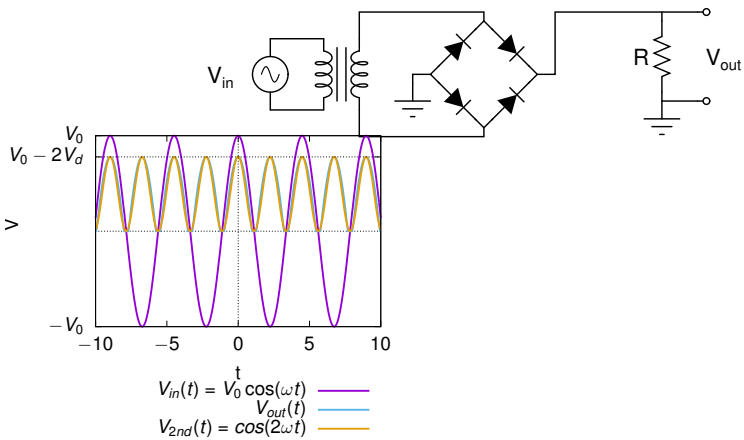
$$\Delta V \leq \frac{V_{max}}{2RCf_{in}}$$

# Full-wave rectifier as Frequency doubler

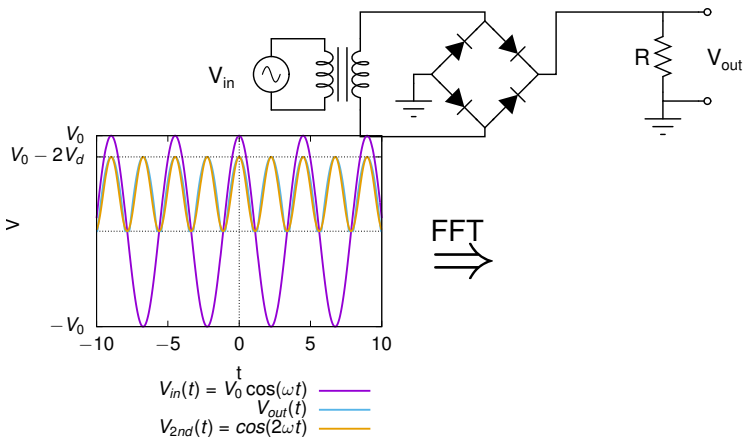




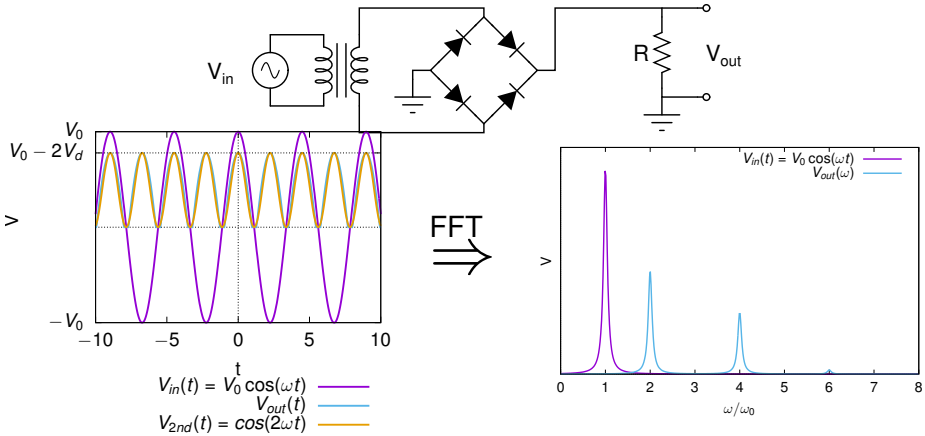
# Full-wave rectifier as Frequency doubler



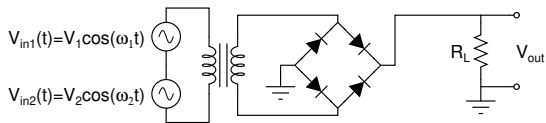
# Full-wave rectifier as Frequency doubler



# Full-wave rectifier as Frequency doubler



# Full-wave rectifier as Frequency adder



$$\begin{aligned} V_{out}(t) &= |V_{in}(t)| = \sqrt{V_{in}^2(t)} = \sqrt{(V_1 \cos(\omega_1 t) + V_2 \cos(\omega_2 t))^2} \\ &= \sqrt{V_1^2 \cos^2(\omega_1 t) + 2V_1 V_2 \cos(\omega_1 t) \cos(\omega_2 t) + V_2^2 \cos^2(\omega_2 t)} \end{aligned}$$

Assuming  $V_1 \gg V_2$

$$\begin{aligned} V_{out}(t) &\approx \sqrt{V_1^2 \cos^2(\omega_1 t) + 2V_1 V_2 \cos(\omega_1 t) \cos(\omega_2 t) + \cancel{V_2^2 \cos^2(\omega_2 t)}} \\ &\approx V_1 \left( \cos(\omega_1 t) + \frac{V_2}{V_1} \cos(\omega_1 t) \cos(\omega_2 t) \right) \\ &\approx V_1 \left( \cos(\omega_1 t) + \frac{V_2}{V_1} \frac{\cos((\omega_1 + \omega_2)t) + \cos((\omega_1 - \omega_2)t)}{2} \right) \end{aligned}$$

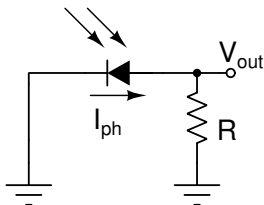
# Light sensing with photodiodes

Photocurrent  $I_{ph}$  proportional to light power  $P_{light}$

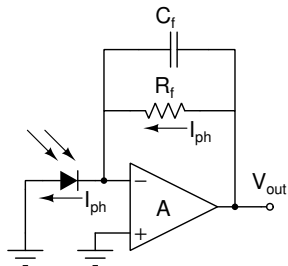
Simple photodiode circuit

Transimpedance amplifier

$$V_{out} = RI_{ph}$$



$$V_{out} = R_f I_{ph}$$



Problems:

- Performance changes with load
- Max output is about  $V_d$