

Transistors

Eugeniy E. Mikhailov

The College of William & Mary



Transistors

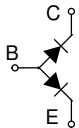
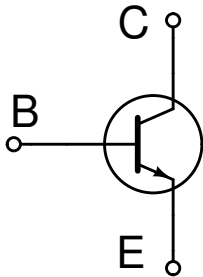
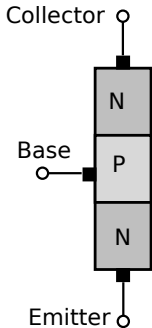
- invented in 1947
- **amplify current**
- lower power consumption
- cheap for mass production
- robust to vibration
- long working time (decades) when properly used
- replaced vacuum tube
- building block of modern electronics

Some areas where vacuum tube are still good

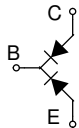
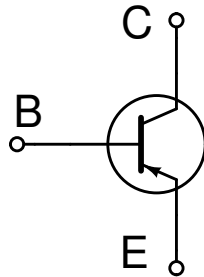
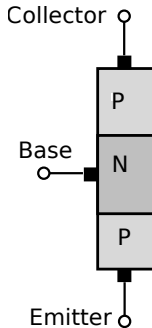
- ultra high voltage applications (more than 1000 V)
- radiation prone locations

Bipolar junction Transistor (BJT)

NPN-transistor

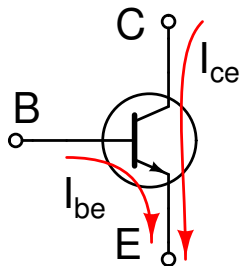


PNP-transistor



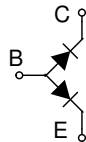
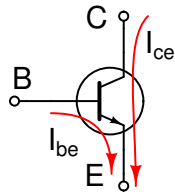
Notation

- Base-emitter current (I_{be})
- Collector-emitter current (I_{ce})
- Base-emitter voltage difference ($V_{be} = V_b - V_e$)
- Collector-emitter voltage difference ($V_{ce} = V_c - V_e$)



Simple NPN-transistor rules

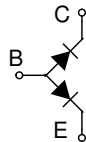
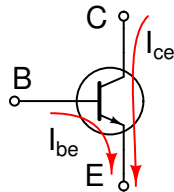
To support shown currents direction



Simple NPN-transistor rules

To support shown currents direction

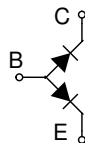
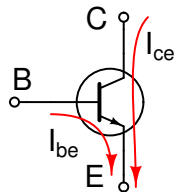
- $V_{ce} > 0$



Simple NPN-transistor rules

To support shown currents direction

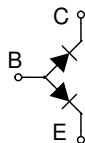
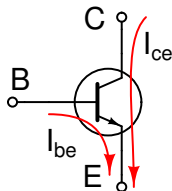
- $V_{ce} > 0$
- $V_{be} > 0$
 - since, it is forward biased diode $V_{be} \approx 0.6 \text{ V}$



Simple NPN-transistor rules

To support shown currents direction

- $V_{ce} > 0$
- $V_{be} > 0$
 - since, it is forward biased diode $V_{be} \approx 0.6 \text{ V}$
- $V_{cb} > 0$
 - since, it is reversed biased diode, no current goes from collector to base, all collector current is directed to emitter
 - if $V_{cb} < 0$ transistor goes to **saturation** and cannot be described by the following simple rule.

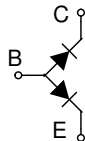
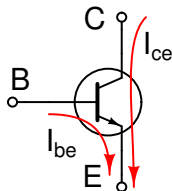


Simple NPN-transistor rules

To support shown currents direction

- $V_{ce} > 0$
- $V_{be} > 0$
 - since, it is forward biased diode $V_{be} \approx 0.6 \text{ V}$
- $V_{cb} > 0$
 - since, it is reversed biased diode, no current goes from collector to base, all collector current is directed to emitter
 - if $V_{cb} < 0$ transistor goes to **saturation** and cannot be described by the following simple rule.

If above holds true then



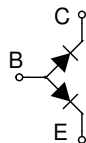
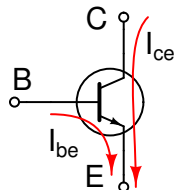
Simple NPN-transistor rules

To support shown currents direction

- $V_{ce} > 0$
- $V_{be} > 0$
 - since, it is forward biased diode $V_{be} \approx 0.6 \text{ V}$
- $V_{cb} > 0$
 - since, it is reversed biased diode, no current goes from collector to base, all collector current is directed to emitter
 - if $V_{cb} < 0$ transistor goes to **saturation** and cannot be described by the following simple rule.

If above holds true then

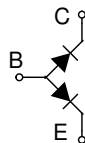
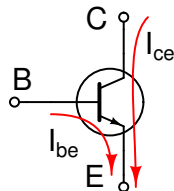
- $I_{ce} = \beta I_{be}$ thus a BJT is a current amplifier



Simple NPN-transistor rules

To support shown currents direction

- $V_{ce} > 0$
- $V_{be} > 0$
 - since, it is forward biased diode $V_{be} \approx 0.6 \text{ V}$
- $V_{cb} > 0$
 - since, it is reversed biased diode, no current goes from collector to base, all collector current is directed to emitter
 - if $V_{cb} < 0$ transistor goes to **saturation** and cannot be described by the following simple rule.



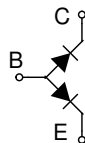
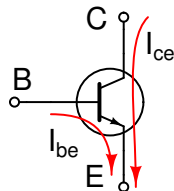
If above holds true then

- $I_{ce} = \beta I_{be}$ thus a BJT is a current amplifier
- *the static forward current transfer ratio*
 β (or sometimes h_{fe}) $\approx 100 \dots 200$

Simple NPN-transistor rules

To support shown currents direction

- $V_{ce} > 0$
- $V_{be} > 0$
 - since, it is forward biased diode $V_{be} \approx 0.6 \text{ V}$
- $V_{cb} > 0$
 - since, it is reversed biased diode, no current goes from collector to base, all collector current is directed to emitter
 - if $V_{cb} < 0$ transistor goes to **saturation** and cannot be described by the following simple rule.



If above holds true then

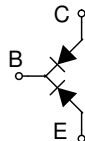
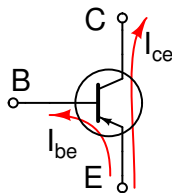
- $I_{ce} = \beta I_{be}$ thus a BJT is a current amplifier
- *the static forward current transfer ratio*
 β (or sometimes h_{fe}) $\approx 100 \dots 200$
- $I_e = I_{be} + I_{ce} = (\beta + 1)I_{be} \approx \beta I_{be}$

Simple PNP-transistor rules

Apply the same rules as before for NPN BJT but multiply currents and voltages by -1 .

Hints

- the arrow indicates the direction in which current is supposed to flow.
- the arrow always connects the base and emitter.



Design considerations for β

Remember β is not a constant!

It depends on many parameters

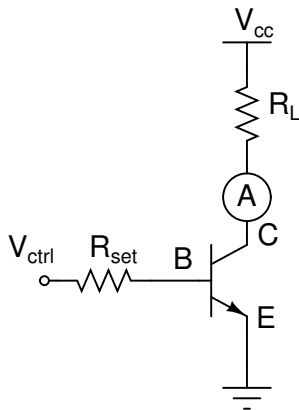
- temperature
- collector current
- varies from device to device even in the same batch

Good design should not depend on β value.

Constant current source

Current through the load resistor does not depend on the load resistance.

$$I_L = I_C = \beta I_{be} = \beta \frac{V_{ctrl} - .6V}{R_{set}}$$

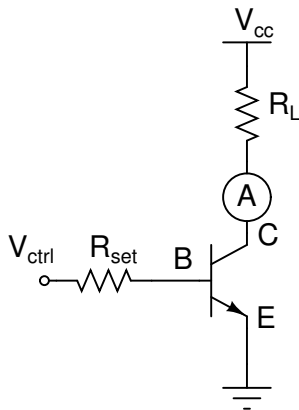


Constant current source

Current through the load resistor does not depend on the load resistance.

$$I_L = I_C = \beta I_{be} = \beta \frac{V_{ctrl} - .6V}{R_{set}}$$

This is actually a sample of **bad design** since the current through the load **depends on β** .



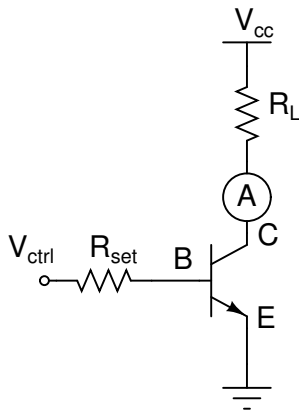
Constant current source

Current through the load resistor does not depend on the load resistance.

$$I_L = I_C = \beta I_{be} = \beta \frac{V_{ctrl} - .6V}{R_{set}}$$

This is actually a sample of **bad design** since the current through the load **depends on β** .

$$V_C = V_{CC} - R_L I_L$$



Constant current source

Current through the load resistor does not depend on the load resistance.

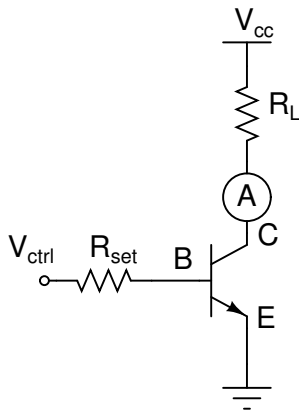
$$I_L = I_C = \beta I_{be} = \beta \frac{V_{ctrl} - .6V}{R_{set}}$$

This is actually a sample of **bad design** since the current through the load **depends on β** .

$$V_C = V_{CC} - R_L I_L$$

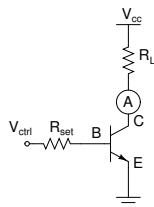
remember that V_C must be $> V_b$ thus current cannot be bigger than the saturation current

$$I_{sat} = \max(I_L) \leq \frac{V_{CC} - V_b}{R_L} \approx \frac{V_{CC}}{R_L}$$

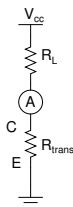


Constant current source (continued)

From V_{CC} point of view, left schematic is equivalent to the right one.



$$R_{trans} = \frac{V_C}{I_L} = \frac{V_{CC} - I_L R_L}{I_L}$$



Transistor

Tran(sform)-(re)sistor

Constant current source. Power dissipation.

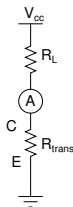
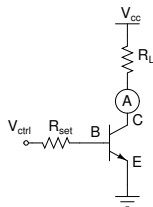
Transistor power dissipation

$$P_{trans} = P_{be} + P_{ce} = V_{be}I_{be} + V_{ce}I_{ce}$$

Since

$$V_{be} \leq V_{ce}, I_{be} = I_{ce}/\beta \ll I_{ce}, \text{ and } I_{ce} = I_L$$

$$P_{trans} \approx V_{ce}I_{ce} = R_{trans}I_L^2$$



Constant current source. Power dissipation.

Transistor power dissipation

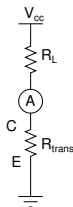
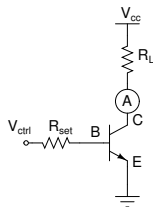
$$P_{trans} = P_{be} + P_{ce} = V_{be}I_{be} + V_{ce}I_{ce}$$

Since

$$V_{be} \leq V_{ce}, I_{be} = I_{ce}/\beta \ll I_{ce}, \text{ and } I_{ce} = I_L$$

$$P_{trans} \approx V_{ce}I_{ce} = R_{trans}I_L^2$$

Maximum power dissipation in transistor



Constant current source. Power dissipation.

Transistor power dissipation

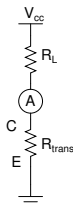
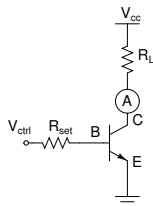
$$P_{trans} = P_{be} + P_{ce} = V_{be}I_{be} + V_{ce}I_{ce}$$

Since

$$V_{be} \leq V_{ce}, I_{be} = I_{ce}/\beta \ll I_{ce}, \text{ and } I_{ce} = I_L$$

$$P_{trans} \approx V_{ce}I_{ce} = R_{trans}I_L^2$$

Maximum power dissipation in transistor is when $R_{trans} = R_L$



Constant current source. Power dissipation.

Transistor power dissipation

$$P_{trans} = P_{be} + P_{ce} = V_{be}I_{be} + V_{ce}I_{ce}$$

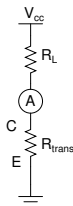
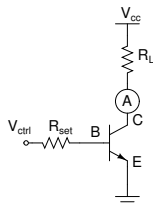
Since

$$V_{be} \leq V_{ce}, I_{be} = I_{ce}/\beta \ll I_{ce}, \text{ and } I_{ce} = I_L$$

$$P_{trans} \approx V_{ce}I_{ce} = R_{trans}I_L^2$$

Maximum power dissipation in transistor is when $R_{trans} = R_L$

$$\max(P_{trans}) = \frac{V_{cc}^2}{4R_L}, \text{ when } I_L = \frac{V_{cc}}{2R_L}$$



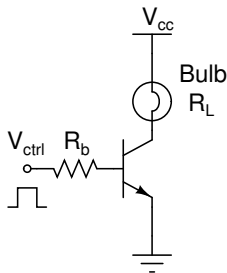
Voltage controlled switch

When properly designed outcome does not depend on reasonable variations of β

Recall that typically $\beta = 100 \dots 200$

We will assume the worst case scenario $\beta = 10$

Notice that R_L limits collector current

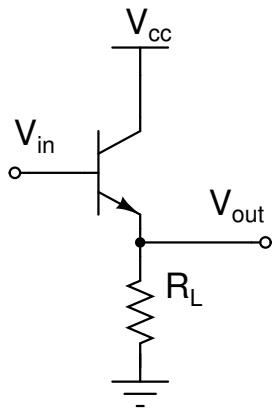


$$I_L = \frac{V_{cc}}{R_L}$$

$$I_{be} = \frac{V_{ctrl} - .6V}{R_b} = \frac{I_L}{\beta}$$

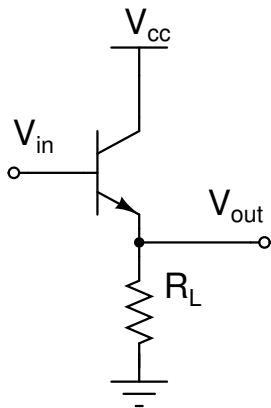
$$R_b \leq \frac{V_{ctrl} - .6V}{V_{cc}} \beta R_L$$

Emitter follower



$$V_{out} = V_{in} - 0.6V$$

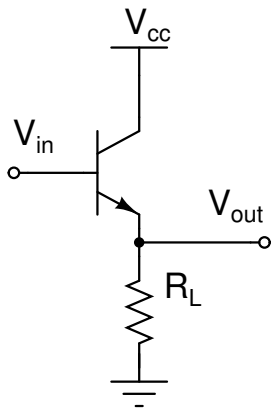
Emitter follower



$$V_{out} = V_{in} - 0.6V$$

Gain. What gain?

Emitter follower



$$V_{out} = V_{in} - 0.6V$$

Gain. What gain?

We achieved the input impedance increase.

$$R_{input} = \frac{V_{in}}{I_{be}} \approx R_L(\beta + 1)$$

As a result our V_{in} source is not overloaded and our load receive all required current (as long as the collector power supply can support it).