

# Transistors applications: AC amplifiers

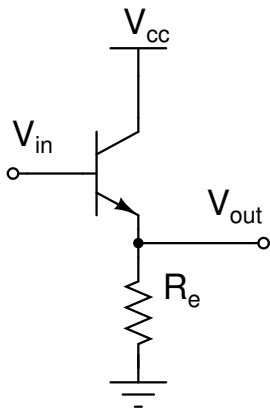
Eugeniy E. Mikhailov

The College of William & Mary



Lecture 07

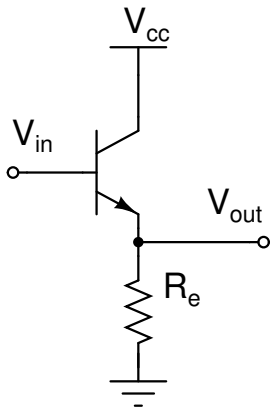
# Summary of simple emitter follower



## Advantages

- input impedance increase  $Z_{in} = \beta R_e$
- power/current gain
- output does not depend on  $\beta$
- simple

# Summary of simple emitter follower



## Advantages

- input impedance increase  $Z_{in} = \beta R_e$
- power/current gain
- output does not depend on  $\beta$
- simple

## Disadvantages

- input signal must be positive
  - even more it should be above 0.6 V
- no voltage gain

# Real life signal

In real life signals usually swing around zero.

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Solution 1: Push-Pull follower

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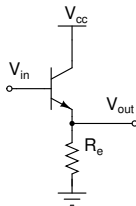
We need to do something with our simple emitter follower.

Solution 1: Push-Pull follower

Solution 2: AC-coupled biased-amplifier

# NPN and PNP emitter follower

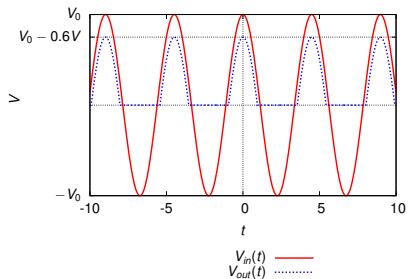
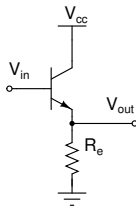
NPN emitter follower





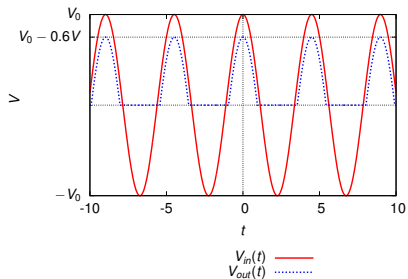
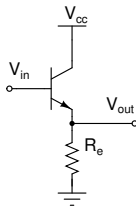
# NPN and PNP emitter follower

NPN emitter follower

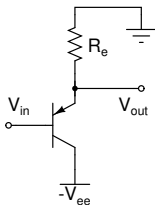


# NPN and PNP emitter follower

NPN emitter follower

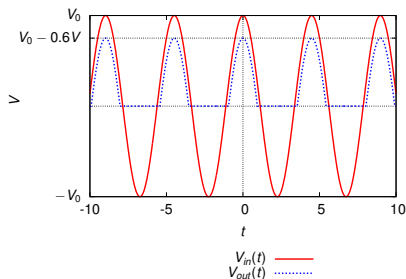
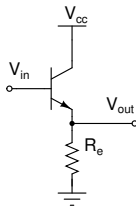


PNP emitter follower

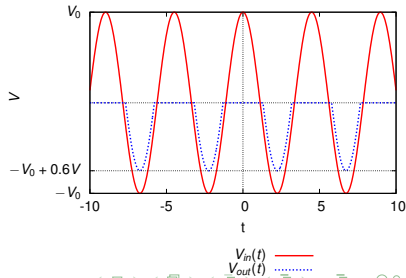
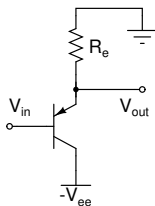


# NPN and PNP emitter follower

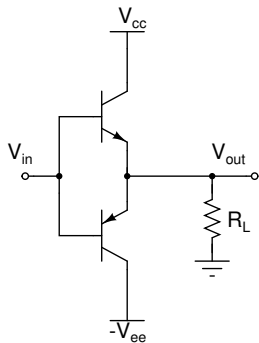
NPN emitter follower



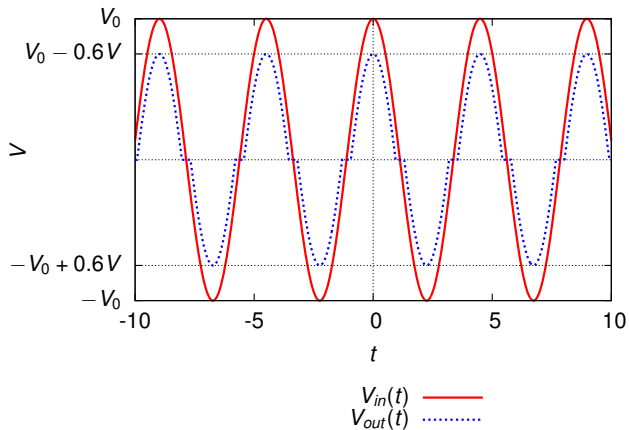
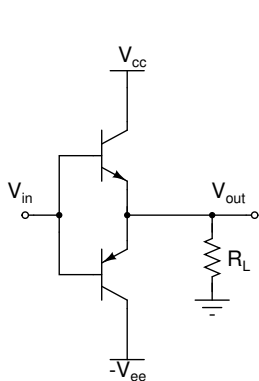
PNP emitter follower



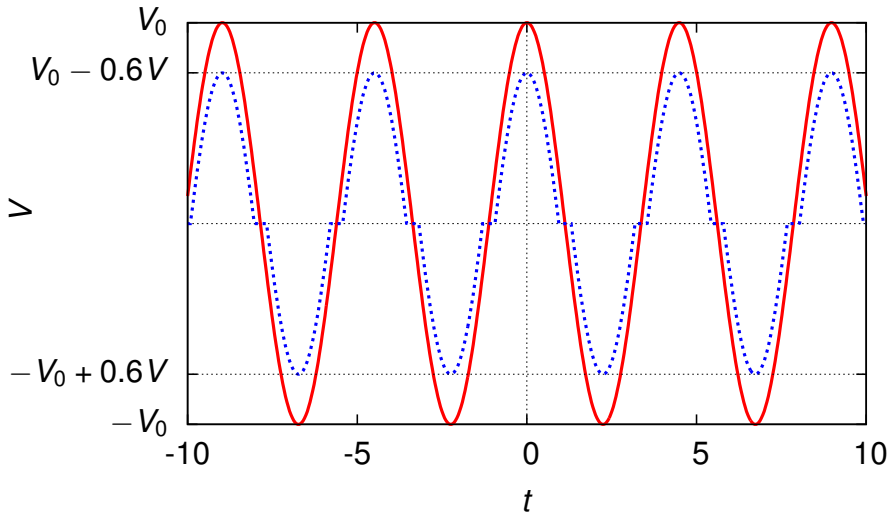
# Push-Pull emitter follower



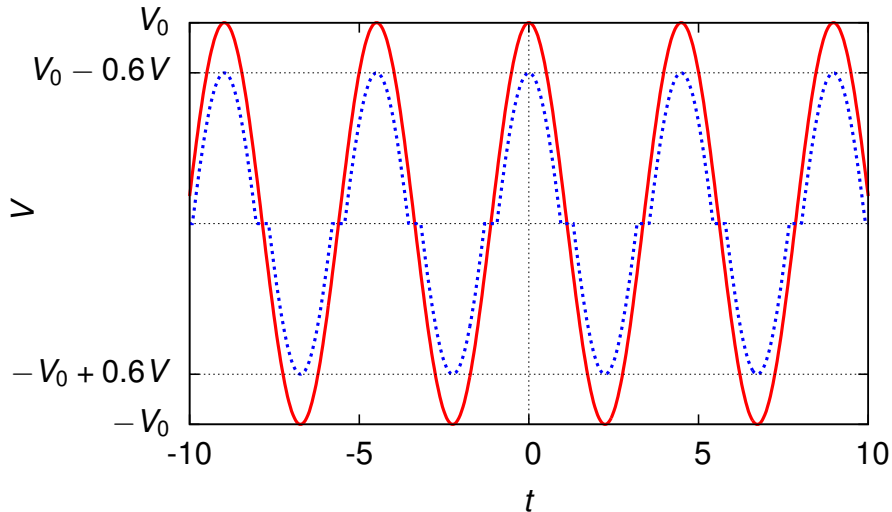
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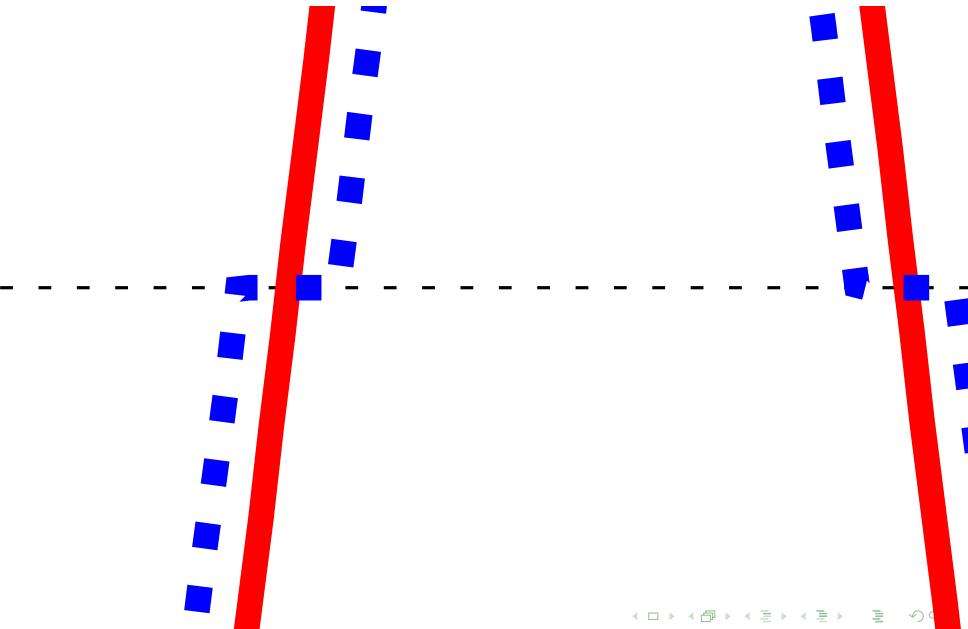
# Push-Pull follower crossovers



# Push-Pull follower crossovers

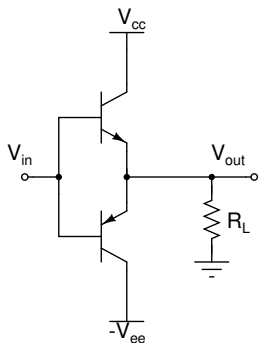


# Push-Pull follower crossovers

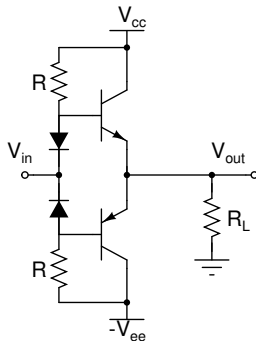
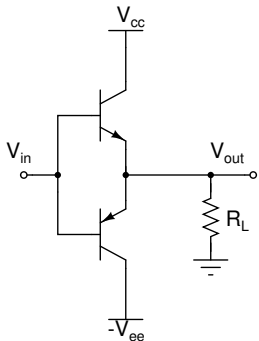




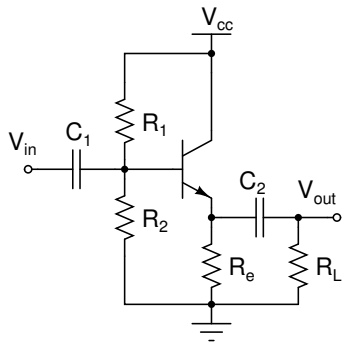
# Push-Pull emitter follower improved



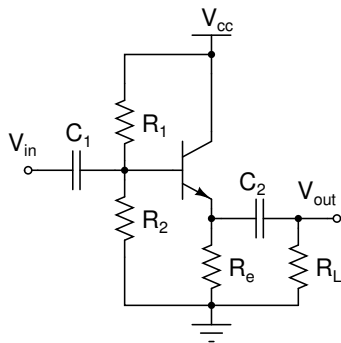
# Push-Pull emitter follower improved



# AC-coupled emitter follower



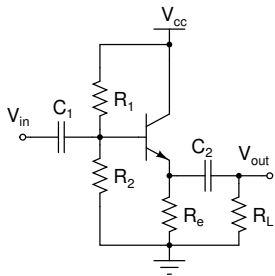
# AC-coupled emitter follower



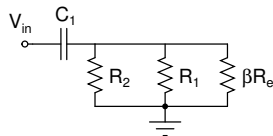
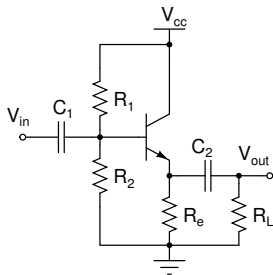
## Design rules

- maximum output swing
  - $V_e = V_{cc}/2$
- disregarding  $V_{be} = 0.6\text{ V}$ 
  - $V_b \approx V_e = V_{cc}/2$
  - thus  $R_1 = R_2$
- quiescent current  $I_e = V_e/R_e$
- we want  $I_{R_1+R_2} \gg I_b$ 
  - factor of 10 for a safe margin
  - $I_{R_1+R_2} \geq 10I_b = 10I_e/\beta$
  - thus  $R_1 = R_2 \leq R_e\beta/10$

# AC-coupled emitter follower: capacitors choice



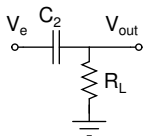
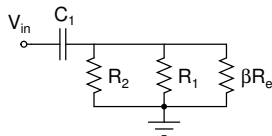
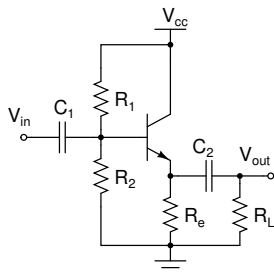
# AC-coupled emitter follower: capacitors choice



From AC point of view

- Input is RC high-pass
  - $C = C_1$
  - $R = R_1 \parallel R_2 \parallel \beta R_e$
  - $f_{3db} = \frac{1}{2\pi} \frac{1}{C_1 (R_1 \parallel R_2 \parallel \beta R_e)}$ 
    - with above rules  $R \approx R_1/2$

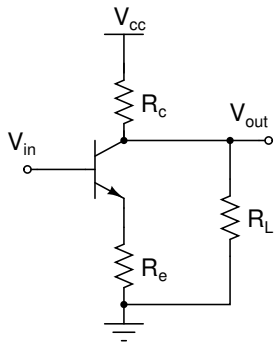
# AC-coupled emitter follower: capacitors choice



From AC point of view

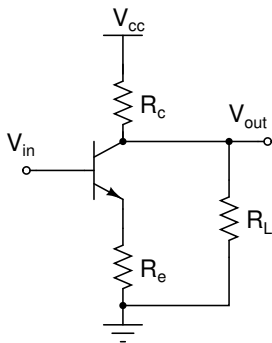
- Input is RC high-pass
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  - $f_{3db} = \frac{1}{2\pi} \frac{1}{C_1 (R_1 \parallel R_2 \parallel \beta R_e)}$ 
    - with above rules  $R \approx R_1/2$
- Output is also RC high-pass
  - $C = C_2$
  - $R = R_L$
  - $f_{3db} = \frac{1}{2\pi} \frac{1}{C_2 R_L}$
  - for unloaded filter  $R_L \gg R_e$ 
    - factor of 10 for a safe margin  
 $R_L = 10R_e$

# Common emitter (inverting) amplifier



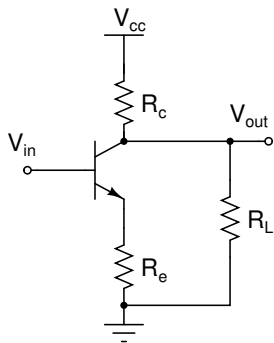


# Common emitter (inverting) amplifier



- $I_C = I_E = (V_{in} - 0.6V)/R_E$
- $V_{out} = V_{CC} - R_C I_C$
- $V_{out} = V_{CC} - R_C (V_{in} - 0.6V)/R_E$
- $V_{out} = (V_{CC} + (0.6V)R_C/R_E) - V_{in}R_C/R_E$
- gain  $G = -R_C/R_E$
- attractive to put  $R_E = 0$ 
  - transistor model fails
  - transistor emitter resistance  
 $r_e = 25mV/I_C$
  - gain  $G = -R_C/r_e$

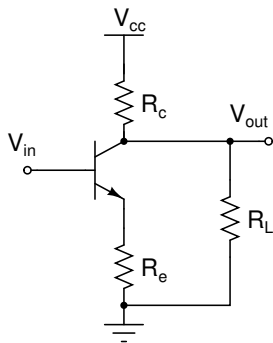
# Common emitter amplifier signal output impedance



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In the pass band we can neglect capacitors

$$\begin{aligned}V_{out} &= V_{CC} - I_C R_C = V_{CC} - (I_{CE} + I_L) R_C \\ &= (V_{CC} - I_{CE} R_C) - I_L R_C \\ &= V_{th} - I_L R_{th}\end{aligned}$$



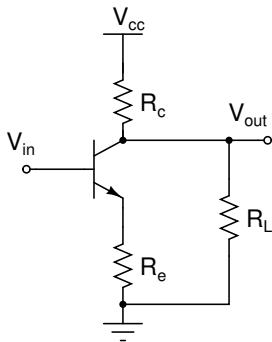
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Thévenin's equivalent

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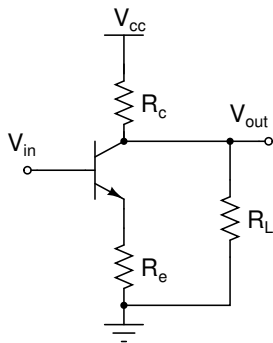
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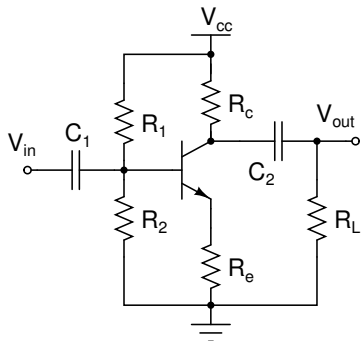
$$\begin{aligned}V_{th} &= V_{CC} - I_{ce} R_C \\ R_{th} &= R_C\end{aligned}$$

Rule of 10 must be satisfied

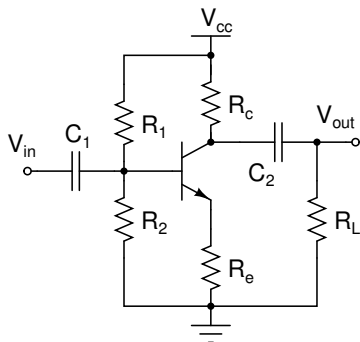
$$R_L \geq 10 R_C$$



# AC-coupled common emitter (inverting) amplifier



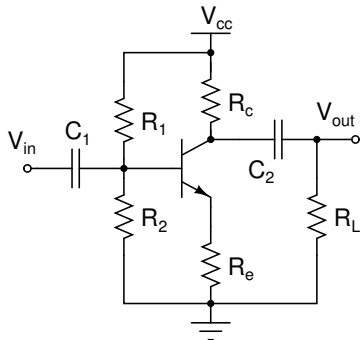
# AC-coupled common emitter (inverting) amplifier



## Design rules

- chose gain  $G = R_c/R_e$
- maximum output swing
  - $V_c = V_{cc}/2$
- quiescent current
  - $I_c = (V_{cc} - V_c)/R_c = V_{cc}/2R_c$
- $R_c = V_{cc}/(2I_c)$
- $R_e = R_c/G$
- we want  $I_{R_1+R_2} \gg I_b$ 
  - factor of 10 for a safe margin
    - $I_{R_1+R_2} \geq 10I_b = 10I_c/\beta$
    - $R_1 + R_2 \leq V_{cc}\beta/(10I_c)$
- $V_b = V_e + 0.6V$
- $R_2/(R_1 + R_2) = V_b/V_{cc}$

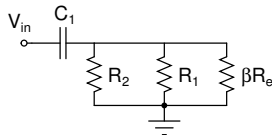
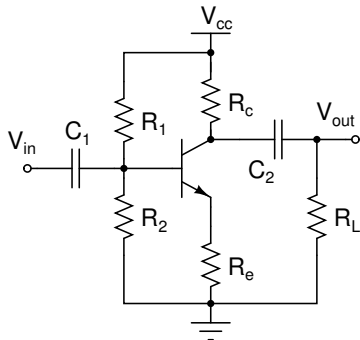
# AC-coupled (inverting) amplifier capacitors choice





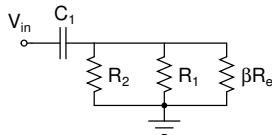
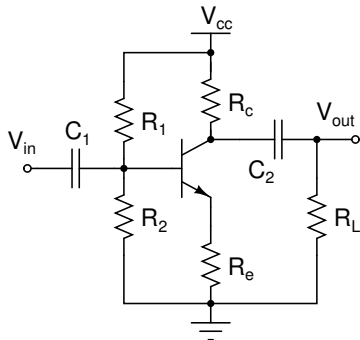
# AC-coupled (inverting) amplifier capacitors choice

Input equivalent

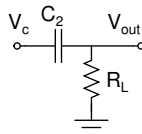


# AC-coupled (inverting) amplifier capacitors choice

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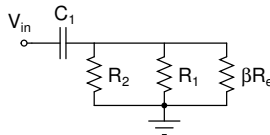
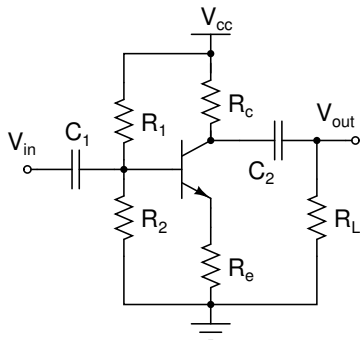


Output equivalent

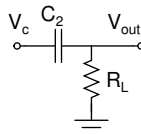


# AC-coupled (inverting) amplifier capacitors choice

Input equivalent



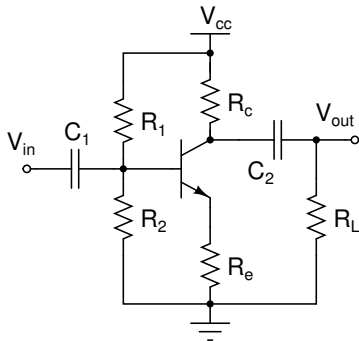
Output equivalent



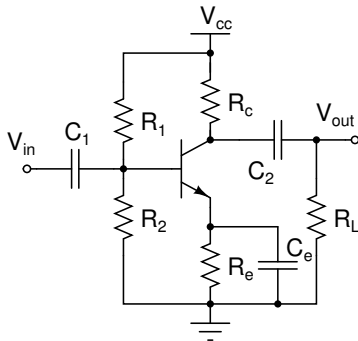
See notes about AC-coupled emitter follower

# AC-coupled (inverting) amplifier with HF gain boost

From



To



Think what happens with equivalent impedance of  $R_e$  at high frequencies