

# Transistors applications: AC amplifiers

Eugeniy E. Mikhailov

The College of William & Mary



Lecture 07

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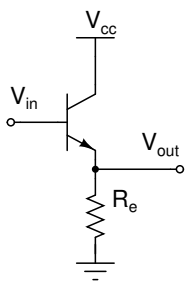
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## Summary of simple emitter follower



### Advantages

- input impedance increase  $Z_{in} = \beta R_e$
- power/current gain
- output does not depend on  $\beta$
- simple

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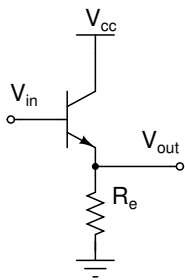
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## Summary of simple emitter follower



### Advantages

- input impedance increase  $Z_{in} = \beta R_e$
- power/current gain
- output does not depend on  $\beta$
- simple

### Disadvantages

- input signal must be positive
  - even more it should be above 0.6 V
- no voltage gain

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## Real life signal

In real life signals usually swing around zero.

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## Real life signal

In real life signals usually swing around zero.

We need to do something with our simple emitter follower.

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## Real life signal

In real life signals usually swing around zero.

We need to do something with our simple emitter follower.

Solution 1: Push-Pull follower

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## Real life signal

In real life signals usually swing around zero.

We need to do something with our simple emitter follower.

Solution 1: Push-Pull follower

Solution 2: AC-coupled biased-amplifier

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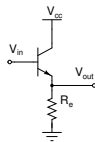
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## NPN and PNP emitter follower

NPN emitter follower



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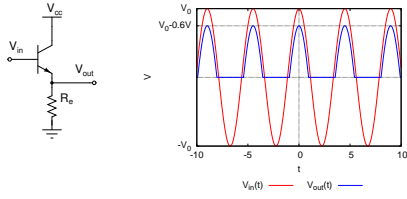
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## NPN and PNP emitter follower

NPN emitter follower



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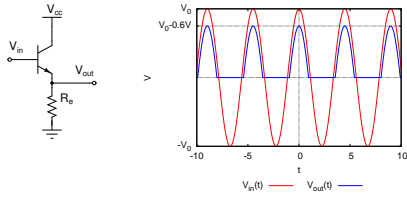
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## NPN and PNP emitter follower

NPN emitter follower



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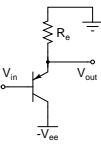
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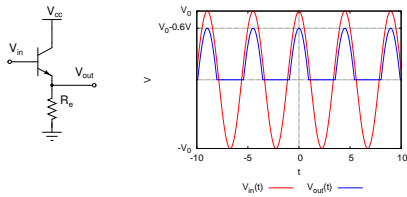
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PNP emitter follower



## NPN and PNP emitter follower

NPN emitter follower



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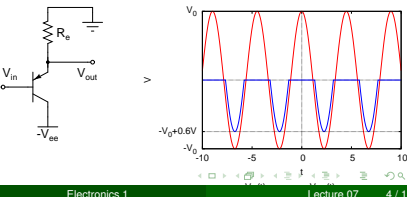
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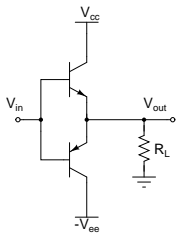
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PNP emitter follower



## Push-Pull emitter follower



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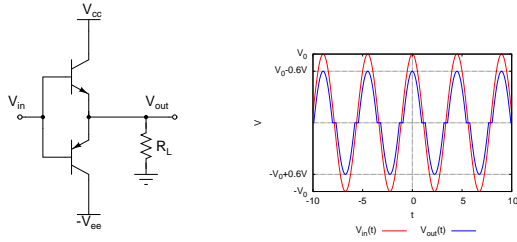
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# Push-Pull emitter follower



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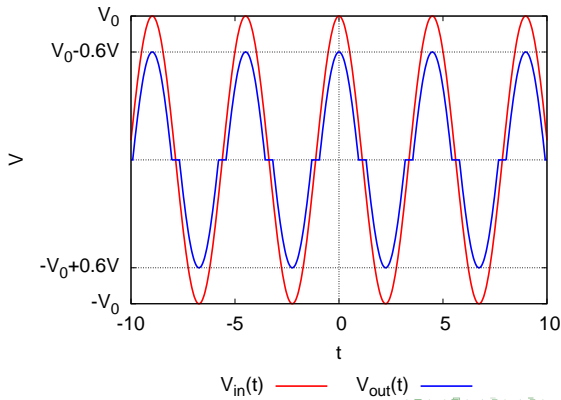
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# Push-Pull follower crossovers



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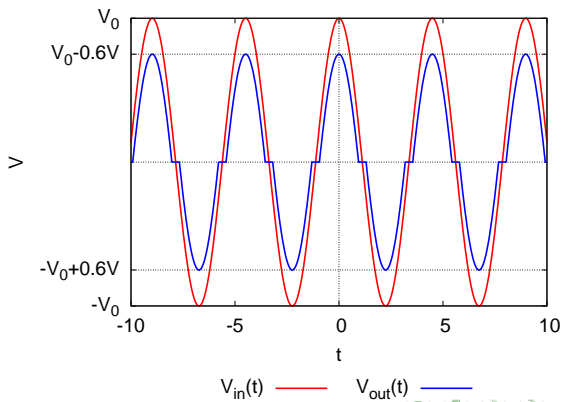
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# Push-Pull follower crossovers



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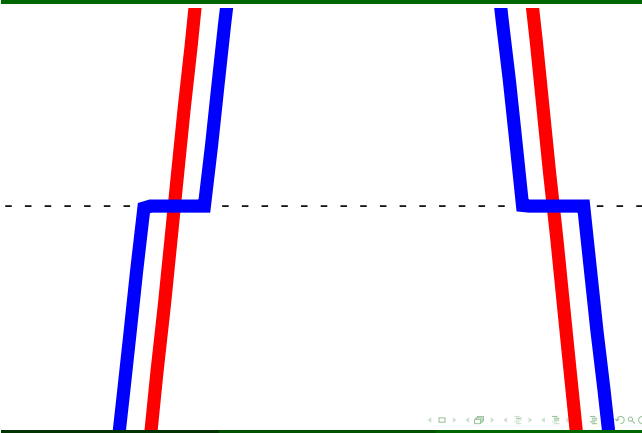
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# Push-Pull follower crossovers



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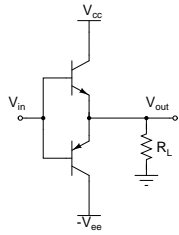
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## Push-Pull emitter follower improved



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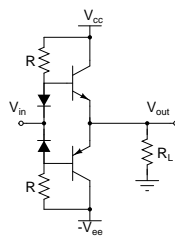
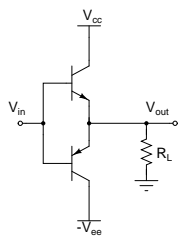
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## Push-Pull emitter follower improved



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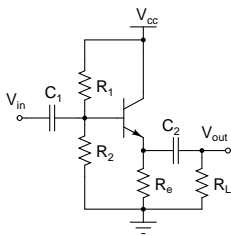
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## AC-coupled emitter follower



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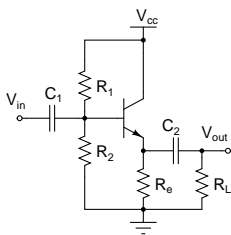
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## AC-coupled emitter follower



### Design rules

- maximum output swing
  - $V_e = V_{cc}/2$
- disregarding  $V_{be} = 0.6\text{ V}$ 
  - $V_b = V_e = V_{cc}/2$
  - thus  $R_1 = R_2$
- quiescent current  $I_e = V_e/R_e$
- we want  $I_{R_1+R_2} \gg I_b$ 
  - factor of 10 for a safe margin
  - $I_{R_1+R_2} = 10I_b = 10I_e/\beta$
  - thus  $R_1 = R_2 = R_e\beta/10$

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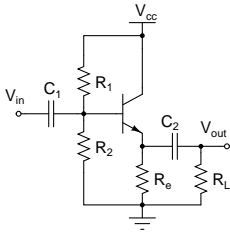
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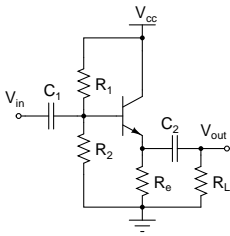
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## AC-coupled emitter follower: capacitors choice

From AC point of view

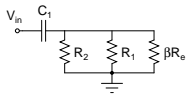


## AC-coupled emitter follower: capacitors choice

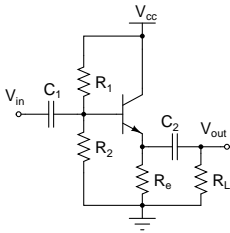


From AC point of view

- Input is RC high-pass
  - $C = C_1$
  - $R = R_1 || R_2 || \beta R_e$
  - $f_{3db} = \frac{1}{2\pi C_1 (R_1 || R_2 || \beta R_e)}$ 
    - with above rules  $R \approx R_1/2$

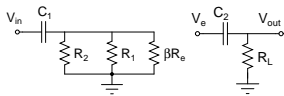


## AC-coupled emitter follower: capacitors choice

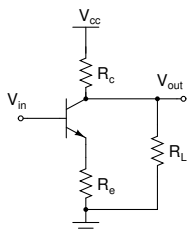


From AC point of view

- Input is RC high-pass
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  - $R = R_1 || R_2 || \beta R_e$
  - $f_{3db} = \frac{1}{2\pi C_1 (R_1 || R_2 || \beta R_e)}$ 
    - with above rules  $R \approx R_1/2$
- Output is also RC high-pass
  - $C = C_2$
  - $R = R_L$
  - $f_{3db} = \frac{1}{2\pi C_2 R_L}$
  - for unloaded filter  $R_L \gg R_e$ 
    - factor of 10 for a safe margin
    - $R_L = 10R_e$



## Common emitter (inverting) amplifier



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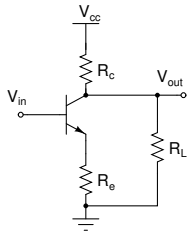
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## Common emitter (inverting) amplifier



- $I_c = I_e = (V_{in} - 0.6V)/R_e$
- $V_{out} = V_{cc} - R_c I_c$
- $V_{out} = V_{cc} - R_c(V_{in} - 0.6V)/R_e$
- $V_{out} = (V_{cc} + (0.6V)R_c/R_e) - V_{in}R_c/R_e$
- gain  $G = -R_c/R_e$
- attractive to put  $R_e = 0$ 
  - transistor model fails
  - transistor emitter resistance
  - $r_e = 25mV/I_c$
  - gain  $G = -R_c/r_e$

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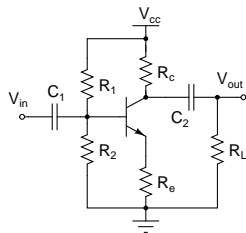
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## AC-coupled common emitter (inverting) amplifier



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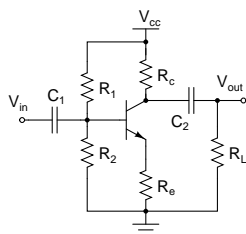
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## AC-coupled common emitter (inverting) amplifier

### Design rules

- chose gain  $G = R_c/R_e$
- maximum output swing
  - $V_c = V_{cc}/2$
- quiescent current
  - $I_c = (V_{cc} - V_c)/R_c = V_{cc}/2R_c$
- $R_c = V_{cc}/(2I_c)$
- $R_e = R_c/G$
- we want  $I_{R1+R2} \gg I_b$ 
  - factor of 10 for a safe margin
  - $I_{R1+R2} = 10I_b = 10I_c/\beta$
  - $R_1 + R_2 = V_{cc}\beta/(10I_c)$
- $V_b = V_e + 0.6$
- $R_2/(R_1 + R_2) = V_b/V_{cc}$



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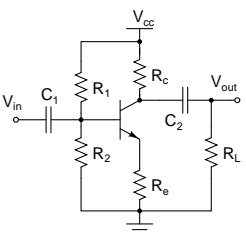
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## AC-coupled (inverting) amplifier signal output impedance



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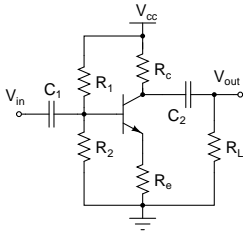
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## AC-coupled (inverting) amplifier signal output impedance

In the pass band we can neglect capacitors



$$\begin{aligned} V_{out} &= V_{cc} - I_c R_c = V_{cc} - (I_{ce} + I_L) R_c \\ &= (V_{cc} - I_{ce} R_c) - I_L R_c \\ &= V_{th} - I_L R_{th} \end{aligned}$$

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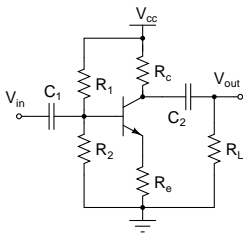
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## AC-coupled (inverting) amplifier signal output impedance

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Thévenin's equivalent

$$\begin{aligned} V_{th} &= V_{cc} - I_{ce} R_c \\ R_{th} &= R_c \end{aligned}$$

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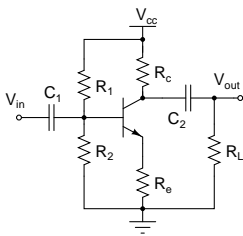
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## AC-coupled (inverting) amplifier signal output impedance

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$$\begin{aligned} V_{out} &= V_{cc} - I_c R_c = V_{cc} - (I_{ce} + I_L) R_c \\ &= (V_{cc} - I_{ce} R_c) - I_L R_c \\ &= V_{th} - I_L R_{th} \end{aligned}$$

Thévenin's equivalent

$$\begin{aligned} V_{th} &= V_{cc} - I_{ce} R_c \\ R_{th} &= R_c \end{aligned}$$

Rule of 10 must be satisfied

$$R_L \geq 10 R_c$$

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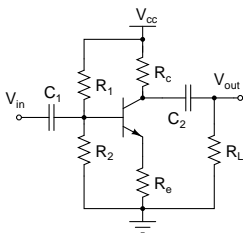
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## AC-coupled (inverting) amplifier capacitors choice



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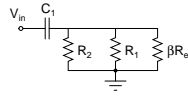
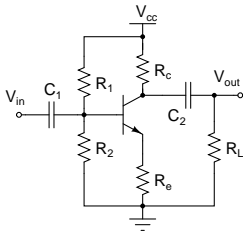
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## AC-coupled (inverting) amplifier capacitors choice

Input equivalent



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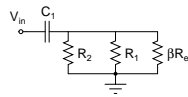
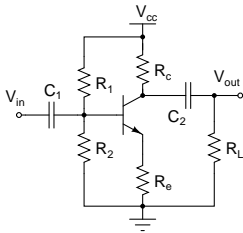
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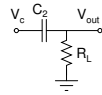
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## AC-coupled (inverting) amplifier capacitors choice

Input equivalent



Output equivalent



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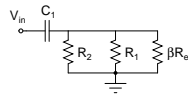
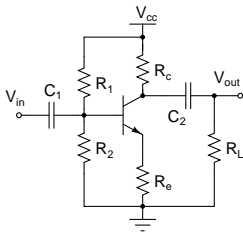
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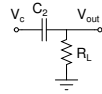
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## AC-coupled (inverting) amplifier capacitors choice

Input equivalent



Output equivalent



See notes about AC-coupled emitter follower

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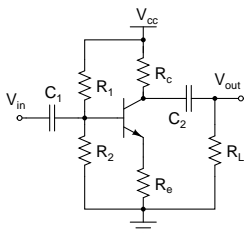
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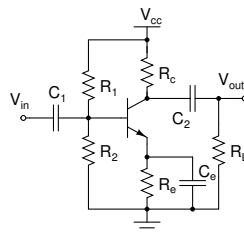
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## AC-coupled (inverting) amplifier with HF gain boost

From



To



Think what happens with equivalent impedance of  $R_e$  at high frequencies

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