

# Transistors.

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The College of William & Mary



Lecture 06

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## Transistors

- invented in 1947
- **amplify current**
- lower power consumption
- cheap for mass production
- robust to vibration
- long working time (decades) when properly used
- replaced vacuum tube
- building block of modern electronics

Some areas where vacuum tube are still good

- ultra high voltage applications (more than 1000 V)
- radiation prone locations

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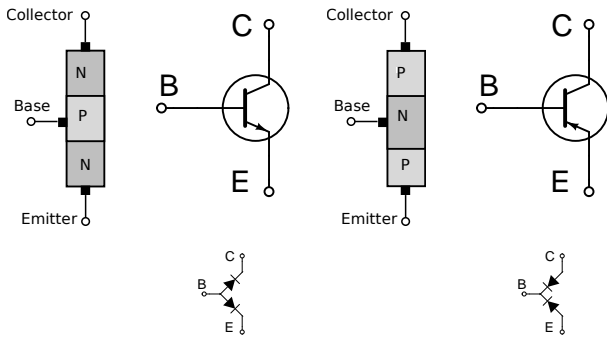
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## Bipolar junction Transistor (BJT)

NPN-transistor

PNP-transistor



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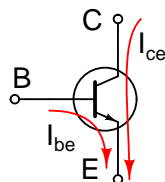
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## Notation

- Base-emitter current ( $I_{be}$ )
- Collector-emitter current ( $I_{ce}$ )
- Base-emitter voltage difference ( $V_{be} = V_b - V_e$ )
- Collector-emitter voltage difference ( $V_{ce} = V_c - V_e$ )



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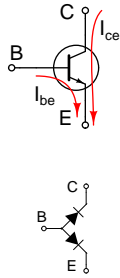
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## Simple NPN-transistor rules

To support shown currents direction



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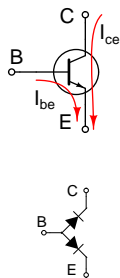
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## Simple NPN-transistor rules

To support shown currents direction

- $V_{ce} > 0$



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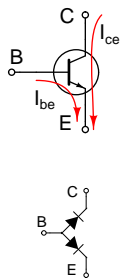
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## Simple NPN-transistor rules

To support shown currents direction

- $V_{ce} > 0$
- $V_{be} > 0$ 
  - since, it is forward biased diode  $V_{be} \approx 0.6 \text{ V}$



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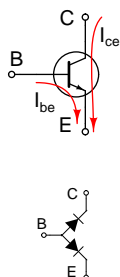
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- $V_{ce} > 0$
- $V_{be} > 0$ 
  - since, it is forward biased diode  $V_{be} \approx 0.6 \text{ V}$
- $V_{cb} > 0$ 
  - since, it is reversed biased diode, no current goes from collector to base, all collector current is directed to emitter
  - if  $V_{cb} < 0$  transistor goes to **saturation** and cannot be described by the following simple rule.



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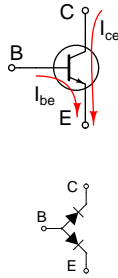
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If above holds true then

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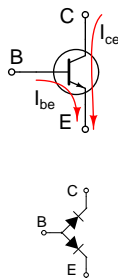
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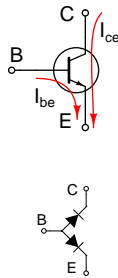
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- $I_{ce} = \beta I_{be}$  thus a BJT is a current amplifier
- *the static forward current transfer ratio*  
 $\beta$  (or sometimes  $h_{fe}$ )  $\approx 100 \dots 200$

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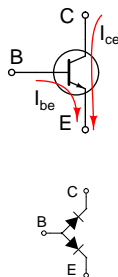
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If above holds true then

- $I_{ce} = \beta I_{be}$  thus a BJT is a current amplifier
- *the static forward current transfer ratio*  
 $\beta$  (or sometimes  $h_{fe}$ )  $\approx 100 \dots 200$
- $I_e = I_{be} + I_{ce} = (\beta + 1)I_{be} \approx \beta I_{be}$

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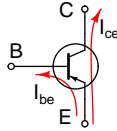
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## Simple PNP-transistor rules

Apply the same rules as before for NPN BJT but multiply currents and voltages by -1.

Hints

- the arrow indicates the direction in which current is supposed to flow.
- the arrow always connects the base and emitter.



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## Design considerations for $\beta$

Remember  $\beta$  is not a constant!

It depends on many parameters

- temperature
- collector current
- varies from device to device even in the same batch

Good design should not depend on  $\beta$  value.

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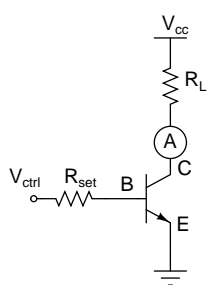
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## Constant current source

Current through the load resistor does not depend on the load resistance.



$$I_L = I_c = \beta I_{be} = \beta \frac{V_{ctrl} - 0.6V}{R_{set}}$$

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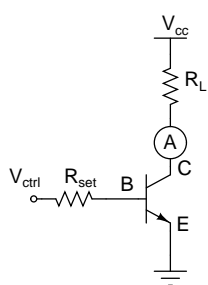
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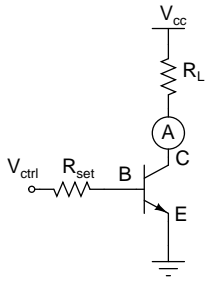
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$$V_c = V_{cc} - R_L I_L$$

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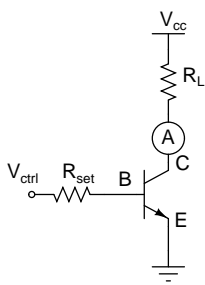
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$$V_c = V_{cc} - R_L I_L$$

remember that  $V_c$  must be  $> V_b$  thus current cannot be bigger then the saturation current

$$I_{sat} = \max(I_L) \leq \frac{V_{cc} - V_b}{R_L} \approx \frac{V_{cc}}{R_L}$$

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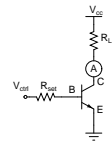
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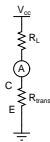
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## Constant current source (continued)

From  $V_{cc}$  point of view, left schematic is equivalent to the right one.



$$R_{trans} = \frac{V_c}{I_L} = \frac{V_{cc} - I_L R_L}{I_L}$$



**Transistor**  
**Tran(sform)-(re)sistor**

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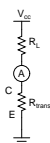
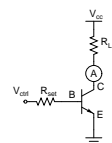
## Constant current source. Power dissipation.

Transistor power dissipation

$$P_{trans} = P_{be} + P_{ce} = V_{be} I_{be} + V_{ce} I_{ce}$$

Since  $V_{be} \leq V_{ce}$ ,  $I_{be} = I_{ce} / \beta \ll I_{ce}$ , and  $I_{ce} = I_L$

$$P_{trans} \approx V_{ce} I_{ce} = R_{trans} I_L^2$$



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## Constant current source. Power dissipation.

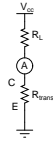
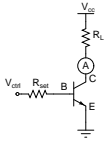
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Maximum power dissipation in transistor



## Constant current source. Power dissipation.

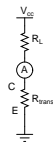
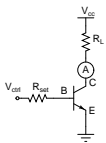
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Maximum power dissipation in transistor is when  $R_{trans} = R_L$



## Constant current source. Power dissipation.

Transistor power dissipation

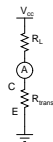
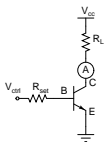
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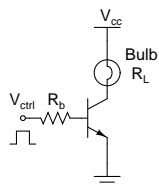
$$\max(P_{trans}) = \frac{V_{cc}^2}{4R_L}, \text{ when } I_L = \frac{V_{cc}}{2R_L}$$



## Voltage controlled switch

When properly designed outcome does not depend on reasonable variations of  $\beta$

Recall that typically  $\beta = 100 \dots 200$   
 We will assume the worst case scenario  $\beta = 10$   
 Notice that  $R_L$  limits collector current

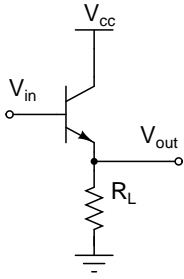


$$I_L = \frac{V_{cc}}{R_L}$$

$$I_{be} = \frac{V_{ctrl} - 0.6V}{R_b} = \frac{I_L}{\beta}$$

$$R_b \leq \frac{V_{ctrl} - 0.6V}{V_{cc}} \beta R_L$$

## Emitter follower



$$V_{out} = V_{in} - 0.6V$$

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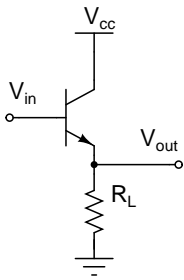
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## Emitter follower



$$V_{out} = V_{in} - 0.6V$$

Gain. What gain?

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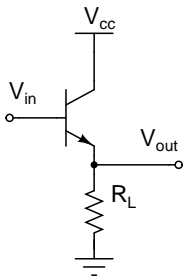
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## Emitter follower



$$V_{out} = V_{in} - 0.6V$$

Gain. What gain?  
We achieved the input impedance increase.

$$R_{input} = \frac{V_{in}}{I_{be}} \approx R_L(\beta + 1)$$

As result our  $V_{in}$  source is not overloaded and our load receive all required current (as long as the collector power supply can support it).

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