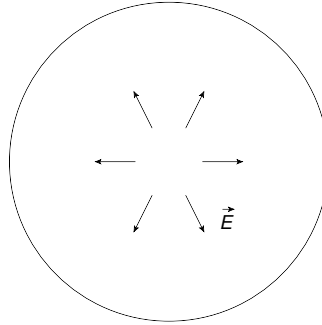


1. For a cylindrical waveguide, the lowest TM mode, the TM_{01} , exhibits a purely outward (or purely inward, depending on the time) electric field in the radial direction. This is very peculiar given that there is no free charge within the waveguide.



(cross section in x-y plane)

Show for this mode, that when thinking properly in 3D, the total flux through a surface surrounding a point on the axis of the waveguide is in fact zero.

As a reminder, you should have in your notes that for the TM_{01} mode,

$$E_z = E_0 J_0(\gamma\rho) e^{i(kz-\omega t)},$$

$$E_\rho = -\frac{ik}{\gamma} E_0 J_1(\gamma\rho) e^{i(kz-\omega t)} \quad (\text{corrected}),$$

$$E_\phi = 0.$$

.....
Say the point of interest on axis is between z_1 and z_2 ($z_2 > z_1$).

Integrate over a closed cylindrical surface of radius r ($r <$ waveguide radius) with endcaps at z_1 and z_2 .

The total flux through the surface is,

$$\oint \vec{E} \cdot \vec{d}a = \int_{\text{curved surface}} E_\rho 2\pi r dz + \int_{(z_2)} E_z 2\pi \rho d\rho - \int_{(z_1)} E_z 2\pi \rho d\rho. \quad (1)$$

Omitting writing the time dependence,

$$\int_{\text{curved surface}} E_\rho 2\pi r dz = -\frac{2\pi ikrE_0}{\gamma} J_1(\gamma\rho) \int_{z_1}^{z_2} e^{ikz} dz = -\frac{2\pi rE_0}{\gamma} J_1(\gamma\rho) (e^{ikz_2} - e^{ikz_1}). \quad (2)$$

Also,

$$\int_{(z_2)} E_z 2\pi \rho d\rho = 2\pi E_0 e^{ikz_2} \int_0^r J_0(\gamma\rho) \rho d\rho = \frac{2\pi E_0}{\gamma} e^{ikz_2} \int_0^r d\rho \frac{d}{d\rho} (\rho J_1(\gamma\rho)) = \frac{2\pi rE_0}{\gamma} J_1(\gamma r) e^{ikz_2}, \quad (3)$$

using the theorem $d[xJ_1(x)]/dx = xJ_0(x)$. Similarly,

$$\int_{(z_1)} E_z 2\pi \rho d\rho = \frac{2\pi rE_0}{\gamma} J_1(\gamma r) e^{ikz_1}. \quad (4)$$

Adding up,

$$\boxed{\oint \vec{E} \cdot \vec{d}a = 0.} \quad (5)$$

2. Jackson problem 8.2.

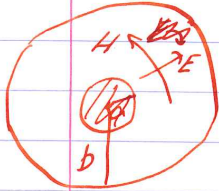
Jackson 8.2

Coaxial waveguide.

Inner radius a , outer radius b ,
metal conductivity σ , skin depth δ .

TEM mode.

"Section 8.1 applies."



a) May solve for $\vec{H} = H_0 \hat{\phi} \frac{a}{\rho} = \vec{H}_t$

Also have $i\omega \vec{E}_t + i\omega \hat{z} \times \vec{B}_t = 0$

$$\begin{aligned} E_t &= -\frac{\omega}{k} \hat{z} \times \mu H_0 = \hat{\rho} \frac{\omega \mu}{k} H_0 \frac{a}{\rho} \\ &= \hat{\rho} \sqrt{\frac{\mu}{\epsilon}} H_0 \frac{a}{\rho} \end{aligned}$$

Propagating vector $\vec{S} = \vec{E} \times \vec{H} = \hat{z} \sqrt{\frac{\mu}{\epsilon}} \frac{a^2}{\rho^2} H_0^2 = \frac{P_{\text{power}}}{\text{Area}}$

Power (instantaneous) $P = \int_{\text{int.}} \vec{S} \cdot d\vec{a} = \int_a^b 2\pi \rho d\rho \sqrt{\frac{\mu}{\epsilon}} \frac{a^2}{\rho^2} H_0^2$
 $= 2\pi a^2 \sqrt{\frac{\mu}{\epsilon}} H_0^2 \ln \frac{b}{a}$

Time average power $P = \langle P \rangle = \sqrt{\frac{\mu}{\epsilon}} \pi a^2 H_0^2 \ln \frac{b}{a}$

b) Above is at some starting z . Now calculate power loss and power attenuation.

From the text $\frac{dP_{\text{loss}}}{dz} = \frac{1}{2\sigma} |H_{\text{nl}}|^2$ (time averaged, where H_{nl} is peak field at relevant surface.)

inside: $\frac{dP_{\text{loss}}}{dz} = \frac{1}{2\sigma} H_0^2$
 $da = 2\pi a dz$

$\therefore \frac{dP_{\text{loss}}}{dz} = \frac{\pi a}{\sigma \delta} H_0^2$

outside: $\frac{dP_{\text{loss}}}{dz} = \frac{\pi b}{\sigma \delta} \frac{a^2}{b^2} H_0^2 = \frac{\pi a^2}{\sigma \delta} \frac{H_0^2}{b}$

total: $-\frac{dP_{\text{loss}}}{dz} = \frac{dP}{dz} = -\frac{\pi a^2}{\sigma \delta} H_0^2 \left(\frac{1}{a} + \frac{1}{b} \right)$

$$\frac{dP}{dz} = -\frac{\pi a^2}{\sigma \delta} \frac{I}{\pi a^2 \mu a} \sqrt{\epsilon'} \left(\frac{1}{a} + \frac{1}{b}\right)$$

$$= -\frac{1}{\sigma \delta} \sqrt{\epsilon'} \frac{(a+b)}{\ln \frac{b}{a}} P = -2\delta P.$$

Hence $P = P_0 e^{-2\delta z}$ and δ is as stated in the problem.

c) $Z_0 = V/I.$

(Ampere) $\vec{H} = \hat{\phi} \frac{I}{2\pi \rho}$

$$\vec{E} = -\frac{\omega \mu}{\rho} \hat{z} \times \vec{H} = \hat{\rho} \sqrt{\frac{\mu}{\epsilon}} |\vec{H}| = \hat{\rho} \sqrt{\frac{\mu}{\epsilon}} \frac{I}{2\pi \rho}$$

$$V = \int_a^b E_\rho d\rho = \sqrt{\frac{\mu}{\epsilon}} \frac{I}{2\pi} \ln \frac{b}{a}$$

$$Z_0 = \frac{V}{I} = \frac{1}{2\pi} \sqrt{\frac{\mu}{\epsilon}} \ln \frac{b}{a}$$

d) resistance per unit length, $\frac{dP}{dz} = -2\delta P = -\langle I^2 \rangle \frac{dR}{dz} = -\frac{1}{2} I^2 \frac{dR}{dz}$

$$P^{\text{avg}} = \sqrt{\frac{\mu}{\epsilon}} \pi a^2 (H_0)^2 \ln \frac{b}{a} = \sqrt{\frac{\mu}{\epsilon}} \pi a^2 \frac{I^2}{4\pi^2 a^2} \ln \frac{b}{a} \quad \text{(time average)}$$

$$P = \frac{1}{4\pi} \sqrt{\frac{\mu}{\epsilon}} I^2 \ln \frac{b}{a} \quad \text{field at inside surface}$$

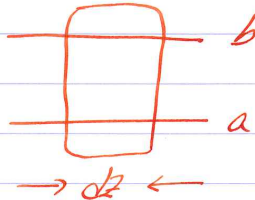
$$\therefore \frac{dR}{dz} = \frac{4P}{I^2} \delta = \frac{1}{\pi} \sqrt{\frac{\mu}{\epsilon}} \ln \frac{b}{a} \cdot \frac{1}{2\sigma \delta} \sqrt{\epsilon'} \frac{(a+b)}{\ln \frac{b}{a}}$$

$$\frac{dR}{dz} = \frac{1}{2\pi \sigma \delta} \left(\frac{1}{a} + \frac{1}{b}\right) \quad \text{(Jackson calls this "R")}$$

d, part 2), inductance per unit length.

Use $\frac{dV}{dz} = -\frac{d}{dz} \frac{dI}{dt}$ and Faraday's law.

Side view, with loop for flux integral:



The loop extends far enough to catch all the flux magnetic field that penetrates the conductors.

$$\mathcal{E} = -L \frac{dI}{dt} = -\frac{d}{dt} \int \vec{B} \cdot d\vec{l} \quad (d\vec{l}) = dz \hat{z}$$

$$\text{Hence,} \quad \frac{dV}{dz} = -\frac{d}{dt} \int B_z dz$$

$$\text{Between} \quad = -\frac{d}{dt} \left\{ \int_a^b B_z dz + \int_0^{\infty} B_z dz + \int_0^{\infty} B_z dz \right\}$$

(inside) outside
($p < a$) $p > b$.

$$\int_a^b B_z dz = \frac{\mu_0 H I}{2\pi} \int_a^b \frac{dz}{z} = \frac{\mu_0 H I}{2\pi} \ln \frac{b}{a} \cdot I$$

$$\int_0^{\infty} B_z dz = \int_0^{\infty} \frac{\mu_0 H I}{2\pi a} e^{-\sqrt{1-i}\sqrt{z/a}} dz = \frac{\mu_0 H I}{2\pi a} \frac{\delta}{1-i}$$

$$= \frac{\mu_0 \delta}{4\pi a} (H I) I$$

$$\text{Only keep real part: } \text{Re} \int_0^{\infty} B_z dz = \frac{\mu_0 \delta}{4\pi a} I$$

Same for outside conductor, with $a \rightarrow b$.

$$\therefore \boxed{\frac{dL}{dz} = \frac{\mu_0 H I}{2\pi} \ln \frac{b}{a} + \frac{\mu_0 \delta}{4\pi} \left(\frac{1}{a} + \frac{1}{b} \right)} \quad (\text{often called this "L"})$$

3. (a) Find for electric dipole radiation in the far zone, also known as the radiation zone and characterized by $r/\lambda \gg 1$, the ratio

$$\frac{|c\vec{B}|}{|\vec{E}|}.$$

(b) Find the same ratio for the near zone, also known as the static zone and characterized by $r/\lambda \ll 1$.

(c & d) Find the same ratio for magnetic dipole radiation in the far and near zones.

.....
For electric radiation,

$$\begin{aligned}\vec{H} &= \frac{ck^2}{4\pi} \frac{e^{ikr}}{r} (\hat{n} \times \vec{p}) \left(1 - \frac{1}{ikr}\right), \\ \vec{E} &= \frac{1}{4\pi\epsilon_0} \left\{ k^2 (\hat{n} \times \vec{p}) \times \hat{n} \frac{e^{ikr}}{r} + e^{ikr} (3\hat{n}(\hat{n} \cdot \vec{p}) - \vec{p}) \left(\frac{1}{r^3} - \frac{ik}{r^2}\right) \right\}.\end{aligned}\quad (6)$$

(a) In the radiation zone ($r \rightarrow \infty$),

$$\begin{aligned}\vec{B} &= \mu_0 \vec{H} = \frac{\mu_0 ck^2}{4\pi} \frac{e^{ikr}}{r} (\hat{n} \times \vec{p}), \\ \vec{E} &= \frac{k^2}{4\pi\epsilon_0} \frac{e^{ikr}}{r} (\hat{n} \times \vec{p}) \times \hat{n}.\end{aligned}\quad (7)$$

Hence

$$\frac{|c\vec{B}|}{|\vec{E}|} = \epsilon_0 \mu_0 c^2 = 1. \quad (8)$$

(b) In the near zone ($r \rightarrow 0$),

$$\begin{aligned}\vec{B} &= \frac{i\mu_0 ck}{4\pi} \frac{e^{ikr}}{r^2} (\hat{n} \times \vec{p}), \\ \vec{E} &= \frac{1}{4\pi\epsilon_0} \frac{e^{ikr}}{r^3} (3\hat{n}(\hat{n} \cdot \vec{p}) - \vec{p}),\end{aligned}\quad (9)$$

so that,

$$\frac{|c\vec{B}|}{|\vec{E}|} = \epsilon_0 \mu_0 c^2 \times \mathcal{O}(kr) \rightarrow 0. \quad (10)$$

(c) and (d), the magnetic cases, are similar, with $\vec{E} \leftrightarrow \pm c\vec{B}$ and $\vec{p} \rightarrow \vec{m}/c$.

(c) is as above, and

(d)

$$\frac{|c\vec{B}|}{|\vec{E}|} = \epsilon_0 \mu_0 c^2 \times \mathcal{O}\left(\frac{1}{kr}\right) \rightarrow \infty. \quad (11)$$